

T. Borkovits¹

Transit timing variations in hierarchical triple (exoplanetary) systems - an analytic study

¹ Baja Astronomical Observatory, Baja

borko@alcyone.bajaobs.hu



MOTIVATION

- Increasing number of exoplanetary systems
- Lengthening time interval of the observations
- Larger sample of dynamically interesting systems (e.g. inclined axis)
- Detection of longer period systems (several months)
- Longer data series \rightarrow possible detection of variations (perturbations)
- More personal motivation:
 - the same effects (and calculations) applied for eclipsing binaries
 - in hierarchical triple stellar systems is interesting for a very few specialists only

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I know, you unterstand what I say



NEW POSSIBILITIES IN O-C ANALYSIS

Detectability of the short period perturbations

o Borkovits et al., 2003: If P'/P <= 100P even the short period perturbations in the eclipsing O—C diagram (i.e. the time-delay in the occurence of the eclipsing minima) may reach 0.001 days \rightarrow theoretically can be detected by ground-based photometry (Perhaps IU Aur?)



The short-term perturbations in the O—C curve produced from a numeric integration of the IU Aur triple system

This valid for an eclipsing binary with typical period of a few days But recently we know transiting exoplanets with periods of months!

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<u>Analytical study on long-term perturbations in hierarchical</u> <u>triple systems with (and without) distorted components</u>

Final purpose:

- Analytical form of the Transit Timing Variation (eclipsing O-C)!

- We must calculate the perturbations in the observational and NOT only
 - in the dynamical frame of reference **DO NOT CONFUSE THE TWO!!!**
- Our final independent variable is the true longitude (u) measured from

the intersection of the binary's orbital plane and the sky, as in the mid-eclipse moment

$$u \approx \pm \frac{\pi}{2} + 2k\pi$$

NEW POSSIBILITIES IN O-C ANALYSIS

<u>Analytical study on long-term perturbations in hierarchical</u> <u>triple systems with (and without) distorted components</u>

- For the analytical form of O-C:

Kepler-equation-"like" =>

 $\Delta e \sim e \left(\frac{P}{D'}\right)^2 u,$

 $\Delta \omega$

$$\int_{t_0}^{t_N} dt = \int_{\pi/2}^{2N\pi + \pi/2} \frac{a^{3/2}}{\mu^{1/2}} \frac{(1 - e^2)^{3/2}}{[1 + e\cos(u - \omega)]^2} \frac{du}{1 - \frac{\rho_1^2}{c_1}\dot{\Omega}\cos i}$$
$$\approx \int \frac{a^{3/2}}{\mu^{1/2}} \frac{(1 - e^2)^{3/2}}{[1 + e\cos(u - \omega)]^2} \left(1 + \frac{\rho_1^2}{c_1}\dot{\Omega}\cos i\right) du.$$
$$\overline{P}_I = \frac{P}{2\pi} \left[2\arctan\left(\sqrt{\frac{1 - e}{1 + e}}\frac{\cos\omega}{1 + \sin\omega}\right) - (1 - e^2)^{1/2}\frac{e\cos\omega}{1 + e\sin\omega}\right]$$
$$\overline{P}_{II} = \frac{P}{2\pi} \left[2\arctan\left(\sqrt{\frac{1 - e}{1 + e}}\frac{-\cos\omega}{1 - \sin\omega}\right) + (1 - e^2)^{1/2}\frac{e\cos\omega}{1 - e\sin\omega}\right]$$

$$\sim \omega \left(\frac{P}{P'}\right)^2 u, \qquad \overline{P}_{II} = \frac{P}{2\pi} \left[2 \operatorname{are} \right]$$

$$\overline{P}_{I,II} = P_{s}E + \frac{P}{2\pi} \left[\pm \frac{1}{2}\pi \mp 2e\cos\omega + \left(\frac{3}{4}e^{2} + \frac{1}{8}e^{4}\right)\sin 2\omega \right]$$
$$\pm \left(\frac{1}{3}e^{3} + \frac{1}{8}e^{5}\right)\cos 3\omega - \frac{5}{32}e^{4}\sin 4\omega \mp \frac{3}{40}e^{5}\cos 5\omega \right]$$

$$u \approx \pm \frac{\pi}{2} + 2k\pi$$

at least some of them:





$$\begin{aligned} \frac{\mathrm{d}a_1}{\mathrm{d}v_2} &= 0, \\ \frac{\mathrm{d}e_1}{\mathrm{d}v_2} &= A_{\mathrm{L}}e_1(1+e_2\cos\nu_2)\left[\left(1-I^2\right)\sin 2g_1\right. \\ &\quad -\frac{1}{2}(1+I)^2\sin(2\nu_2-2\nu_{2\mathrm{m}}-2g_1) \\ &\quad +\frac{1}{2}(1-I)^2\sin(2\nu_2-2\nu_{2\mathrm{m}}+2g_1)\right], \\ \frac{\mathrm{d}\omega_1}{\mathrm{d}v_2} &= A_{\mathrm{L}}(1+e_2\cos\nu_2)\left\{\frac{3}{5}\left(I^2-\frac{1}{3}\right) \\ &\quad +\left(1-I^2\right)\left[\cos 2g_1+\frac{3}{5}\cos(2\nu_2-2\nu_{2\mathrm{m}})\right] \\ &\quad +\frac{1}{2}(1+I)^2\cos(2\nu_2-2\nu_{2\mathrm{m}}-2g_1) \\ &\quad +\frac{1}{2}(1-I)^2\cos(2\nu_2-2\nu_{2\mathrm{m}}+2g_1)\right\} \\ &\quad -\frac{\mathrm{d}\Omega_1}{\mathrm{d}v_2}\cos i_1, \end{aligned}$$

0

PERTURBATION EQUATIONS – short-term terms

and, finally, the direct terms are as follows:

$$\frac{\mu_{1}^{1/2}}{a_{1}^{3/2}} \left(\dot{u}_{1p} \right)_{dir}^{-1} = A_{L} (1 + e_{2} \cos \nu_{2}) \left\{ \frac{4}{5} \left(I^{2} - \frac{1}{3} \right) f_{1}(e_{1}) + \frac{51}{20} \left(1 - I^{2} \right) e_{1}^{2} f_{2}(e_{1}) \cos 2g_{1} + \frac{4}{5} \left(1 - I^{2} \right) f_{1}(e_{1}) \cos (2\nu_{2} - 2\nu_{2m}) + \frac{51}{40} (1 + I)^{2} e_{1}^{2} f_{2}(e_{1}) \cos (2\nu_{2} - 2\nu_{2m} - 2g_{1}) + \frac{51}{40} (1 - I)^{2} e_{1}^{2} f_{2}(e_{1}) \cos (2\nu_{2} - 2\nu_{2m} + 2g_{1}) \right\},$$
(15)

where

$$A_{\rm L} = \frac{15}{8} \frac{m_3}{m_{123}} \frac{P_1}{P_2} \frac{(1 - e_1^2)^{1/2}}{(1 - e_2^2)^{3/2}},\tag{16}$$

and

$$f_1(e) = 1 + \frac{25}{8}e^2 + \frac{15}{8}e^4 + \frac{95}{64}e^6, \tag{17}$$

$$f_2(e) = 1 + \frac{31}{51}e^2 + \frac{23}{48}e^4.$$
(18)

Furthermore, i_m denotes the mutual inclination of the two orbital planes, while

 $I = \cos i_{\rm m},\tag{19}$

and m_{123} stands for the total mass of the system.

and the result:

$$\begin{aligned} -C_{P_2} &= \frac{P_1}{2\pi} A_L \left\{ \left(I^2 - \frac{1}{3} \right) \frac{4}{5} \left(1 \mp \frac{3}{2} e_1 \sin \omega_1 \right) \mathcal{M} \right. \\ &+ \left(1 - I^2 \right) \frac{2}{5} \left(1 \mp \frac{3}{2} e_1 \sin \omega_1 \right) \mathcal{S}(2\nu_2 - 2\nu_{2m}) \\ &\mp \left(1 - I^2 \right) 2e_1 \sin(\omega_1 - 2g_1) \mathcal{M} \\ &\pm (1 + I)^2 \frac{1}{2} e_1 C(2\nu_2 - 2\nu_{2m} + \omega_1 - 2g_1) \\ &\mp (1 - I)^2 \frac{1}{2} e_1 C(2\nu_1 - 2\nu_{2m} - \omega_1 + 2g_1) \\ &+ \cot i_1 \sin i_m \left[-I \frac{2}{5} \left(1 \mp 2e_1 \sin \omega_1 \right) \cos u_{1m} \mathcal{M} \right. \\ &+ (1 + I) \frac{1}{10} (1 \mp 2e_1 \sin \omega_1) \mathcal{S}(2\nu_2 - 2\nu_{2m} + u_{1m}) \\ &- (1 - I) \frac{1}{10} (1 \mp 2e_1 \sin \omega_1) \mathcal{S}(2\nu_2 - 2\nu_{2m} - u_{1m}) \right] \right\} \end{aligned}$$

where

 $+\mathcal{O}(e_1^2),$

$$\mathcal{M} = \int 1 + e_2 \cos \nu_2 d\nu_2 = \nu_2 - l_2 + e_2 \sin \nu_2$$
(21)

$$= 3e_2 \sin \nu_2 - \frac{3}{4}e_2^2 \sin 2\nu_2 + \frac{1}{3}e_2^3 \sin 3e_2 + \mathcal{O}(e_2^4), \qquad (22)$$

(20)

furthermore,

$$S(x) = \sin(x) + e_2 \sin(x - \nu_2) + \frac{1}{3}e_2 \sin(x + \nu_2), \qquad (23)$$

$$C(x) = \cos(x) + e_2 \cos(x - \nu_2) + \frac{1}{3}e_2 \cos(x + \nu_2).$$
(24)

DISCUSSION – with illustration on COROT-9B

Combination of short-period dynamic and pure geometric (LITE) effects on the O–C curve of CoRoT-9b

 $m_{star} = 0.99 m_{Sun} m_{planet} = 0.0008 m_{Sun} P_{1} = 95^{d} P_{2} = 10,000^{d}$



 $m_{3} = 1.0 m_{Sun}$

 $m_{3} = 0.01 m_{Sun}$

Physical and orbital parameter of CoRoT-9b and its host star from Deeg et al. 2010, Nature

at least some of them:

$$\frac{du_{1}}{dg_{1}} = \frac{1}{A + B\cos 2g_{1}} - \frac{d\Omega_{1}}{dg_{1}}\cos i_{1},$$

$$\frac{da_{1}}{dg_{1}} = 0,$$

$$\frac{1}{e_{1}}\frac{de_{1}}{dg_{1}} = \frac{A_{1}\sin 2g}{A + B\cos 2g},$$

$$\frac{dh_{1}}{dg_{1}} = -\frac{1}{\cos j_{1}}\frac{A_{n1} - A_{n2}\cos 2g}{A + B\cos 2g},$$

$$\cot j_{1}\frac{dj_{1}}{dg_{1}} = \frac{-A_{n2}\sin 2g}{A + B\cos 2g},$$

$$\frac{d\omega_{1}}{dg_{1}} = 1 + \frac{dh_{1}}{dg_{1}}\cos j_{1} - \frac{d\Omega_{1}}{dg_{1}}\cos i_{1},$$

$$\frac{d\Omega_{1}}{dg_{1}} = \frac{dh_{1}}{dg_{1}}\frac{\sin j_{1}}{\sin i_{1}}\cos u_{m} + \frac{dj_{1}}{dg_{1}}\frac{1}{\sin i_{1}}\sin u_{m},$$

$$\frac{di_{1}}{dg_{1}} = -\frac{dh_{1}}{dg_{1}}\sin j_{1}\sin u_{m} + \frac{dj_{1}}{dg_{1}}\cos u_{m},$$
while for the direct term

$$\frac{\mu_1^{1/2}}{a_1^{3/2}} \left(\dot{u}_1 \right)_{\rm dir}^{-1} = \frac{A_{\rm d} + B_{\rm d} \cos 2g}{A + B \cos 2g},$$



where

$$A = A_{\mathbf{G}}(1 - e_1^2)^{-1} \left[I^2 - \frac{1}{5}(1 - e_1^2) + \frac{2}{5} \left(1 + \frac{3}{2}e_1^2 \right) \frac{G_1}{G_2} I \right],$$

$$B = A_{\mathbf{G}}(1 - e_1^2)^{-1} \left[1 - e_1^2 - I^2 - e_1^2 \frac{G_1}{G_2} I \right],$$

Solutions:

Restrictions:
Second order perturbing function (in a₁/a₂ ratio)
Very strong hierarchicity (i. e. G₁/G₂ is negligible)
Point masses

The Hamiltonian does not depend on neither any of the elements of the third companion, nor H_1 .

$$(1 - 5\cos 2g)(\eta - 1)\left(\eta - \theta^2\right) + 4\frac{\theta^2}{\eta_{1/5}}\left(\eta_{1/5} - \eta\right) = 0,$$

where
$$\eta = 1 - e^2,$$
$$\theta = \frac{H_1}{L_1}.$$

Solutions:

Analytical solution of:

$$\frac{\mathrm{d}\zeta}{\mathrm{d}u} = \mp A_{\mathrm{G}} \frac{2}{\mathrm{S}} \sqrt{6} \sqrt{4\zeta^3 - g_2 \zeta - g_3},$$

is Weierstrass elliptic funtion.

whe

$$\begin{aligned} \sigma_{\text{re:}} & \zeta = \eta - \frac{1}{9} \left(5 + 5\theta^2 + \eta_0 \right) \\ g_2 &= \frac{20}{3} \left[\left(\frac{5}{9} \left(1 + \theta^2 \right) - \frac{7}{9} \eta_0 \right) \left(1 + \theta^2 \right) + \frac{19}{45} \eta_0^2 - \theta^2 \right], \\ g_3 &= \frac{1000}{729} \left(1 + \theta^2 \right)^3 - \frac{700}{243} \eta_0 \left(1 + \theta^2 \right)^2 + \frac{20}{27} \left(\frac{11}{9} \eta_0^2 - 5\theta^2 \right) \left(1 + \theta^2 \right) + \frac{32}{27} \left(5\theta^2 + \frac{7}{27} \eta_0^2 \right) \eta_0 \end{aligned}$$

(See Kozai 1962, Söderhjelm 1982 for details)

Not really practical for our purpose

Solutions:

Approximative solution for some centuries:

$$\eta = \frac{1}{2} \left(1 + \theta^{2} \right) + \frac{1}{2} \frac{Z}{x} - \frac{1}{2x} \sqrt{\left[Z - (X + Y) x \right]^{2} - 4XYx(x - x_{0})}, \text{ where:} \qquad \begin{array}{l} X = \eta_{g0} - 1, \\ Y = \eta_{g0} - \theta^{2}, \\ Z = \frac{4}{5} \frac{\theta^{2}}{\eta_{15}} = \frac{XY}{\eta_{g0} - \eta_{15}} x_{0} \end{array}$$

$$\eta^{1/2} = \eta_{g0}^{1/2} + \frac{1}{2} \eta_{g0}^{-1/2} \frac{XY}{B(x_{0})}(x - x_{0}) + \frac{1}{8} \eta_{g0}^{-3/2} \frac{XY}{B(x_{0})} \frac{4\eta_{g0}XYx_{0} + \left[4\eta_{g0}(X + Y) - XY\right]B(x_{0})}{B(x_{0})^{2}}(x - x_{0})^{2} + ..., \\ e = e_{g0} - \frac{1}{2}e_{g0}^{-1} \frac{XY}{B(x_{0})}(x - x_{0}) - \frac{1}{8}e_{g0}^{-2} \frac{XY}{B(x_{0})} \frac{4e_{g0}^{2}XYx_{0} + \left[4e_{g0}^{2}(X + Y) + XY\right]B(x_{0})}{B(x_{0})^{2}}(x - x_{0})^{2} + ..., \\ A_{0} \frac{du}{dg} = \frac{\eta_{g0}^{1/2}}{B(x_{0})} + \frac{1}{2}\eta_{g0}^{-1/2} \frac{4\eta_{g0}XYx_{0} + \left[XY + 2\eta_{g0}(X + Y)\right]B(x_{0})}{B(x_{0})^{3}}(x - x_{0}) \\ + \frac{1}{8}\eta_{g0}^{-3/2} \left\{ \frac{48\eta_{g0}^{2}X^{2}Y^{2}x_{0}^{2} + \left[48\eta_{g0}^{2}(X + Y)Xy_{0} + 12\eta_{g0}X^{2}Y^{2}x_{0}\right]B(x_{0})}{B(x_{0})^{5}} + \frac{\left[8\eta_{g0}^{2}(X + Y)^{2} + 16\eta_{g0}^{2}XY - X^{2}Y^{2} + 8XY\eta_{g0}(X + Y)\right]B(x_{0})^{2}}{B(x_{0})^{5}} \right\}(x - x_{0})^{2} \\ \text{Note:} \quad \left(\frac{du}{dg}\right)_{0} = A_{0}^{-1} \frac{\eta_{0}^{3/2}}{\theta^{2} - \frac{1}{2}\eta_{g0}^{2/2} + (\eta_{g0}^{2} - \theta^{2})\cos 2g_{0}} \right$$

Solutions:

Approximative solution for some centuries:

Solutions:

Restrictions:

•Second order perturbing function (in a_1/a_2 ratio)

Radial tidal forces in the close binary, mass-point ternary
Constant angular velocity vectors

As far as the orbital elements on the r.h.s. of perturbation eqs. can be treated as constants, there closed form solutions.

$$g = \arctan\left[\sqrt{\frac{1+E_0}{1-E_0}}\tan(W_0 + \Pi_0 u)\right],$$

$$e = e_0 + \frac{1}{2}e_0\frac{A_{r1t}}{B}\ln\left[\frac{1-E_0\cos(2W_0 + 2\Pi_0 u)}{1-E_0\cos 2W_0}\right],$$

$$h = h_0 + 2\pi\chi_0 u + \kappa_0\left\{\arctan\left[\sqrt{\frac{1+E_0}{1-E_0}}\tan(W_0 + \Pi_0 u)\right] - \arctan\left[\sqrt{\frac{1+E_0}{1-E_0}}\tan W_0\right]\right\},$$

$$u - u_0 = \frac{1}{2\pi}\frac{1}{A_0}\frac{1}{\sqrt{1-E_0^2}}(W - W_0)$$

Solutions:

 For large mutual inclination the eccentricity cannot be treated as constant. At a relatively close system with medium eccentricity the convergence is very weak, so we need to calculate for higher orders. E.g. here I give the form of the angular velocity of the apsidal motion up to fifth order in e:

$$\begin{split} \Pi^{*} &= \Pi \left\{ 1 + \left[\frac{1}{2} \frac{F_{0}}{1 - E_{0}^{2}} (1 - N_{0}) + \frac{1}{8} \frac{F_{0}}{1 - E_{0}^{2}} X_{1} - \frac{1}{8} \frac{G_{0}}{1 - E_{0}^{2}} - \frac{1}{4} \frac{F_{0}^{2}}{(1 - E_{0}^{2})^{2}} - \frac{1}{4} Y_{1} (1 - N_{0}) - \frac{1}{8} Y_{1} X_{1} - \frac{1}{8} Y_{2} + \frac{1}{8} \frac{F_{0}}{1 - E_{0}^{2}} Y_{1} + \frac{1}{8} Y_{1}^{2} \right] E_{0}^{2} + \\ &+ \left[\frac{7}{32} \frac{F_{0}}{1 - E_{0}^{2}} (1 - N_{0})^{3} + \frac{19}{128} \frac{F_{0}}{1 - E_{0}^{2}} X_{1} (1 - N_{0})^{2} + \frac{3}{64} \frac{F_{0}}{1 - E_{0}^{2}} X_{1}^{2} (1 - N_{0}) + \frac{3}{512} \frac{F_{0}}{1 - E_{0}^{2}} X_{1}^{3} - \frac{19}{128} \frac{G_{0}}{1 - E_{0}^{2}} (1 - N_{0})^{2} - \\ &- \frac{9}{64} \frac{G_{0}}{0 - E_{0}^{2}} X_{1} (1 - N_{0}) - \frac{21}{512} \frac{G_{0}}{1 - E_{0}^{2}} X_{1}^{2} - \frac{45}{128} \frac{F_{0}^{2}}{(1 - E_{0}^{2})^{2}} (1 - N_{0})^{2} - \frac{49}{428} \frac{F_{0}^{2}}{(1 - E_{0}^{2})^{2}} X_{1} (1 - N_{0}) - \frac{21}{512} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} X_{1}^{2} - \\ &- \frac{1}{64} \frac{F_{0}G_{0}}{(1 - E_{0}^{2})^{2}} (1 - N_{0}) + \frac{3}{128} \frac{F_{0}G_{0}}{(1 - E_{0}^{2})^{2}} X_{1}^{3} - \frac{3}{512} \frac{G_{0}^{2}}{(1 - E_{0}^{2})^{2}} X_{1}^{2} - \\ &- \frac{1}{312} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} (1 - N_{0}) + \frac{3}{128} \frac{F_{0}G_{0}}{(1 - E_{0}^{2})^{2}} X_{1} - \frac{3}{512} \frac{G_{0}}{(1 - E_{0}^{2})^{2}} X_{1}^{2} - \\ &- \frac{1}{312} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} (1 - N_{0})^{2} - \frac{9}{128} X_{1} Y_{2} (1 - N_{0}) - \frac{21}{512} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} X_{1}^{2} + \\ &- \frac{1}{2} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} (1 - N_{0})^{2} - \frac{9}{128} X_{1} Y_{2} (1 - N_{0}) - \frac{21}{732} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} X_{1}^{2} + \\ &- \frac{1}{2} \frac{F_{0}}}{(1 - E_{0}^{2})^{2}} (1 - N_{0}) - \frac{5}{16} \frac{F_{0}^{2}}{(1 - E_{0}^{2})^{2}} X_{1} + \frac{3}{12} \frac{F_{0}}{(1 - E_{0}^{2})^{2}} - \\ &- \frac{3}{64} \frac{F_{0}}}{1 - E_{0}^{2}} X_{1} + \left[\frac{1}{8} \frac{F_{0}}}{1 - E_{0}^{2}} Y_{1} (1 - N_{0}) + \frac{3}{52} \frac{F_{0}}}{1 - E_{0}^{2}} X_{1} (1 - N_{0})^{2} - \\ &- \frac{3}{32} X_{1} Y_{1} (1 - N_{0}) - \frac{3}{32} \frac{Y_{1}}}{(1 - N_{0})^{2}} - \\ &- \frac{1}{64} \frac{F_{0}}}{1 - E_{0}^{2}} X_{1} (1 - N_{0}) - \frac{3}{32} \frac{Y_{1}}}{(1 - N_{0})^{2}} - \\ &- \frac{1}{64} \frac{F_{0}}}{1 - E_$$

$$\begin{split} &-\frac{1}{32}\frac{F_0^2}{(1-E_0^2)^2}X_1^2 - \frac{7}{96}\frac{F_0G_0}{(1-E_0^2)^2}(1-N_0) + \frac{1}{192}\frac{F_0G_0}{(1-E_0^2)^2}X_1 - \frac{1}{192}\frac{G_0^2}{(1-E_0^2)^2} + \frac{1}{16}Y_1(1-N_0)^3 - \frac{1}{96}X_1Y_1(1-N_0)^2 - \\ &-\frac{1}{192}X_1^3Y_1 - \frac{1}{96}Y_2(1-N_0)^2 - \frac{7}{192}X_1^2Y_2\Big]\mathcal{E}_0^2\Big)\mathcal{E}_0^2\cos 4g_0 + \\ &+ \left\{\frac{1}{24}\frac{F_0}{1-E_0^2}(1-N_0)^2 - \frac{1}{32}\frac{F_0}{1-E_0^2}X_1(1-N_0) + \frac{1}{192}\frac{F_0}{1-E_0^2}X_1^2 + \frac{1}{32}\frac{G_0}{1-E_0^2}(1-N_0) - \frac{1}{64}\frac{G_0}{1-E_0^2}X_1 + \\ &+ \frac{1}{24}\frac{F_0^2}{(1-E_0^2)^2}(1-N_0) - \frac{1}{48}\frac{F_0^2}{(1-E_0^2)^2}X_1 - \frac{1}{96}\frac{F_0G_0}{(1-E_0^2)^2} - \frac{1}{24}Y_1(1-N_0)^2 + \frac{1}{32}X_1Y_1(1-N_0) - \frac{1}{192}X_1^2Y_1 + \\ &+ \frac{1}{24}\frac{F_0}{(1-E_0^2)^2}(1-N_0) - \frac{1}{48}\frac{F_0^2}{(1-E_0^2)^2}X_1 - \frac{1}{96}\frac{F_0G_0}{(1-E_0^2)^2} - \frac{1}{24}Y_1(1-N_0) - \frac{1}{96}\frac{F_0}{1-E_0^2}X_1Y_1 - \frac{1}{64}\frac{F_0}{1-E_0^2}Y_2 + \frac{5}{192}\frac{G_0}{1-E_0^2}Y_1 + \\ &+ \frac{1}{32}Y_2(1-N_0) - \frac{1}{64}X_1Y_2 - \frac{1}{32}\frac{F_0^3}{(1-E_0^2)}X_1^2(1-N_0)^2 - \frac{5}{1536}\frac{F_0}{1-E_0^2}X_1^3(1-N_0) + \frac{5}{768}\frac{G_0}{1-E_0^2}(1-N_0)^3 + \\ &+ \frac{1}{(-\frac{13}{384}\frac{F_0}{1-E_0^2}}X_1(1-N_0)^3 - \frac{1}{64}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) - \frac{25}{1536}\frac{F_0}{1-E_0^2}X_1^3(1-N_0) + \frac{5}{768}\frac{G_0}{1-E_0^2}(1-N_0)^3 + \\ &+ \frac{17}{1024}\frac{G_0}{1-E_0^2}X_1(1-N_0)^3 + \frac{7}{1768}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) - \frac{25}{256}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) + \frac{1}{3072}\frac{F_0}{1-E_0^2}X_1^3 - \frac{1}{168}\frac{G_0}{1-E_0^2}(1-N_0)^3 + \\ &+ \left[-\frac{1}{64}\frac{F_0}{1-E_0^2}(1-N_0)^3 + \frac{11}{768}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) - \frac{25}{256}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) + \frac{1}{322}\frac{F_0^2}{(1-E_0^2)^2}X_1(1-N_0) + \frac{1}{768}\frac{G_0}{1-E_0^2}(1-N_0)^2 + \\ &+ \frac{3}{256}\frac{G_0}{1-E_0^2}X_1(1-N_0)^3 + \frac{11}{768}\frac{F_0}{1-E_0^2}X_1^2(1-N_0)^2 - \frac{1}{256}\frac{F_0}{1-E_0^2}X_1^2(1-N_0) + \frac{1}{322}\frac{F_0^2}{(1-E_0^2)^2}X_1(1-N_0) + \\ &- \frac{1}{3072}\frac{F_0}{1-E_0^2}X_1(1-N_0)^2 + \frac{3}{256}X_1Y_2(1-N_0)^2 + \frac{3}{256}X_1Y_2(1-N_0)^2 + \frac{1}{325}\frac{F_0}{(1-E_0^2)^2}X_1(1-N_0) + \\ &- \frac{1}{3072}\frac{F_0}{1-E_0^2}X_1(1-N_0)^2 + \frac{3}{256}X_1Y_2(1-N_0) - \frac{7}{37072}\frac{F_0}{1-E_0^2}X_1^2(1-N_0)^2 + \frac{1}{256}\frac{F_0}{1-E_0^2}X_1(1$$

 $\frac{2\pi}{P}O$

Solutions:

- Perturbed form of O-C:

$$\int \frac{a^{3/2}}{\mu^{1/2}} \frac{(1-e^2)^{3/2}}{[1+e\cos(u-\omega)]^2} \,\mathrm{d}u$$

Includes long-term perturbations in all the orbital elements, as well as direct perturbations in mean motion

$$\int \frac{a^{3/2}}{\mu^{1/2}} \frac{(1-e^2)^{3/2}}{[1+e\cos(u-\omega)]^2} \frac{\rho_1^2}{c_1} \dot{\Omega} \cos i du$$

$$\begin{aligned} -C &= V_{100} \cos[\omega_{0} + (1 + \mathcal{U})\Pi(u - u_{0})] + V_{200} \sin[2\omega_{0} + (2 + 2\mathcal{U})\Pi(u - u_{0})] + V_{300} \cos[3\omega_{0} + (3 + 3\mathcal{U})\Pi(u - u_{0})] + \\ + V_{101} \cos[\omega_{0} + h_{0} + (1 + \mathcal{U} + \mathcal{H})\Pi(u - u_{0})] + V_{10-1} \cos[\omega_{0} - h_{0} + (1 + \mathcal{U} - \mathcal{H})\Pi(u - u_{0})] + \\ + V_{102} \cos[\omega_{0} + 2h_{0} + (1 + \mathcal{U} + 2\mathcal{H})\Pi(u - u_{0})] + V_{10-2} \cos[\omega_{0} - h_{0} + (1 + \mathcal{U} - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{103} \cos[\omega_{0} + 3h_{0} + (1 + \mathcal{U} + 3\mathcal{H})\Pi(u - u_{0})] + V_{10-2} \cos[\omega_{0} - h_{0} + (1 + \mathcal{U} - 3\mathcal{H})\Pi(u - u_{0})] + \\ + V_{120} \cos[3\omega_{0} - u_{m0} + (3 + \mathcal{U})\Pi(u - u_{0})] + V_{12-0} \cos[\omega_{0} - 2u_{m0} + (1 - \mathcal{U})\Pi(u - u_{0})] + \\ + V_{121} \cos[3\omega_{0} - u_{m0} + h_{0} + (3 + \mathcal{U} + \mathcal{H})\Pi(u - u_{0})] + V_{12-1} \cos[3\omega_{0} - u_{m0} - h_{0} + (3 + \mathcal{U} - \mathcal{H})\Pi(u - u_{0})] + \\ + V_{122} \cos[3\omega_{0} - u_{m0} + h_{0} + (1 - \mathcal{U} - \mathcal{H})\Pi(u - u_{0})] + V_{12-2} \cos[3\omega_{0} - u_{m0} - h_{0} + (3 + \mathcal{U} - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{122} \cos[3\omega_{0} - u_{m0} + 2h_{0} + (3 + \mathcal{U} + 2\mathcal{H})\Pi(u - u_{0})] + V_{12-2} \cos[3\omega_{0} - u_{m0} - 2h_{0} + (3 + \mathcal{U} - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{122} \cos[3\omega_{0} - u_{m0} + 3h_{0} + (3 + \mathcal{U} + 3\mathcal{H})\Pi(u - u_{0})] + V_{12-2} \cos[3\omega_{0} - u_{m0} - 2h_{0} + (3 + \mathcal{U} - 3\mathcal{H})\Pi(u - u_{0})] + \\ + V_{123} \cos[3\omega_{0} - u_{m0} + 3h_{0} + (3 + \mathcal{U} + 3\mathcal{H})\Pi(u - u_{0})] + V_{12-3} \cos[3\omega_{0} - u_{m0} - 2h_{0} + (3 + \mathcal{U} - 3\mathcal{H})\Pi(u - u_{0})] + \\ + V_{123} \cos[3\omega_{0} - u_{m0} + 3h_{0} + (1 - \mathcal{U} - 3\mathcal{H})\Pi(u - u_{0})] + V_{12-3} \cos[\omega_{0} - 2u_{m0} + 3h_{0} + (1 - \mathcal{U} + 3\mathcal{H})\Pi(u - u_{0})] + \\ + V_{201} \sin[2\omega_{0} + h_{0} + (2 + 2\mathcal{U} + \mathcal{H})\Pi(u - u_{0})] + V_{12-1} \sin[2\omega_{0} - h_{0} + (2\partial_{0} + 2\mathcal{U} - \mathcal{H})\Pi(u - u_{0})] + \\ + V_{202} \sin[2\omega_{0} + 2h_{0} + (2 + 2\mathcal{U} + 2\mathcal{H})\Pi(u - u_{0})] + V_{20-1} \sin[2\omega_{0} - 3h_{0} + (2 + 2\mathcal{U} - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{202} \sin[2\omega_{0} - 2u_{m0} + (4 + 2\mathcal{U})\Pi(u - u_{0})] + V_{2-1} \sin[2\omega_{0} - 3h_{0} + (2 + 2\mathcal{U} - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{202} \sin[2\omega_{0} - 2u_{m0} + h_{0} + (2 + 2\mathcal{H})\Pi(u - u_{0})] + V_{2-2} \sin[2u_{0} - 2h_{0} + (2 - 2\mathcal{H})\Pi(u - u_{0})] + \\ + V_{202} \sin[2\omega_{0} - 2u_{m$$

Mutual inclination: 20 deg





Mutual inclination: 60 deg





Mutual inclination: 89 deg





<u>Analytical study on long-term perturbations in hierarchical</u> <u>triple systems with distorted components -</u> <u>Conclusions, future steps</u>

Perturbations force significant variations in the apsidal motion period, as well as in eccentricity

- → new terms with large amplitude in the O-C curve, which should be considered at the determination of the speed of the apsidal motion (which sometimes determined simply from the slope of the observed short section of the O-C curve
- → variation of eccentricity can be determined from spectroscopy and/or accurate photometry. Combining these with the O-C the spatial orientation of the orbits might be calculated

Next step: to formulate the expressions for practical use (everything is ready for this).

THANK YOU FOR YOUR ATTENTION!



borko@alcyone.bajaobs.hu